



EXPERIMENTAL AND EMPIRICAL
EVALUATION OF THE ANNUAL
EFFICIENCY FOR A TRANS-
CRITICAL R744 BOOSTER SYSTEM
IN ASIAN CLIMATE CONDITIONS

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Motivation



Motivation of the study

Eco-efficiency study

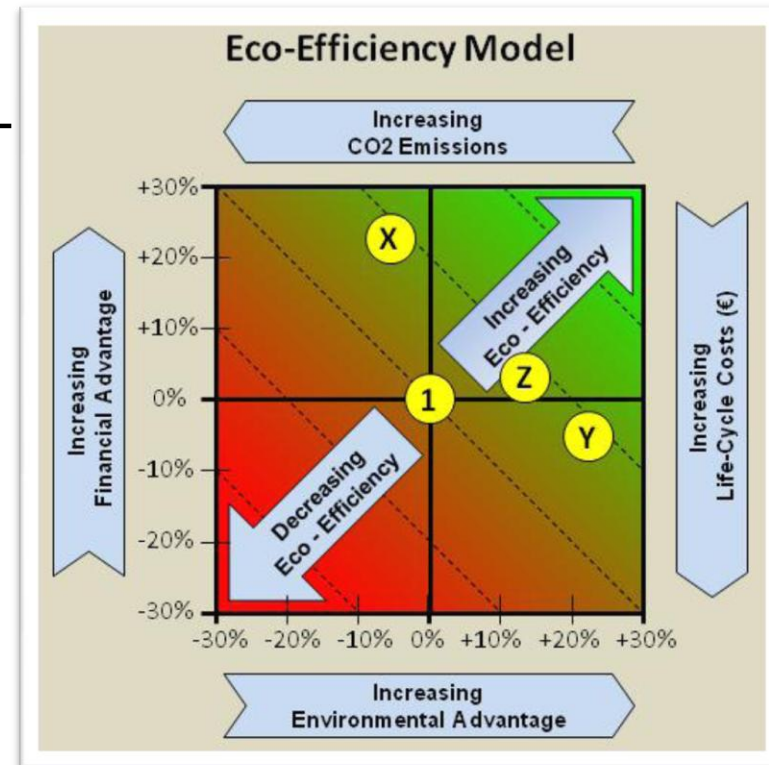
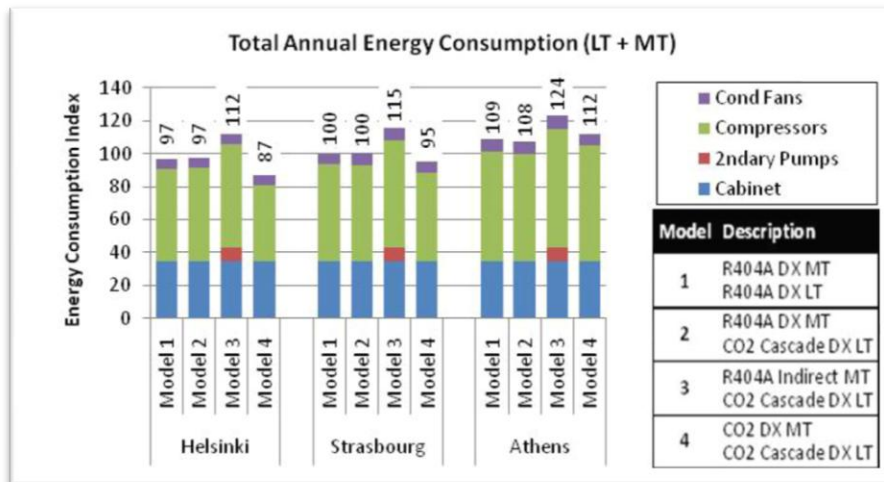
Analytical comparison of supermarket refrigeration systems

/ R404A DX MT - R404A DX LT

/ R404A DX MT - CO₂ Cascade DX LT

/ R404A Indirect MT - CO₂ Cascade DX LT

/ CO₂ DX MT - CO₂ Cascade DX LT

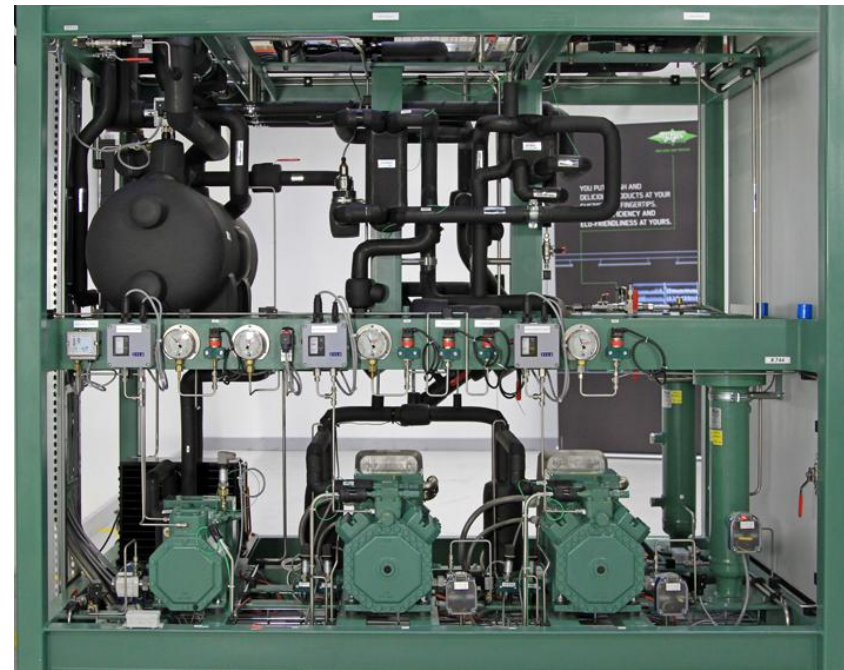


* Thurnham, Timothy 2010, Eco-Efficiency Study of Supermarket Refrigeration, SKM Enviros, London

Experimental and empirical study of a CO₂ booster system

Applied CO₂ booster system

- / State-of-the-art CO₂ booster system of the 2nd generation
 - Oil management, flash gas bypass, IHX (flash gas ↔ liquid)
 - Water-cooled co-axial gas cooler allows the simulation of various ambient conditions
 - Without heat reclaim, parallel compression, two-stage gas cooler and peak load unit
- / Realistic MT / LT load simulation by means of electrical heaters



Reference



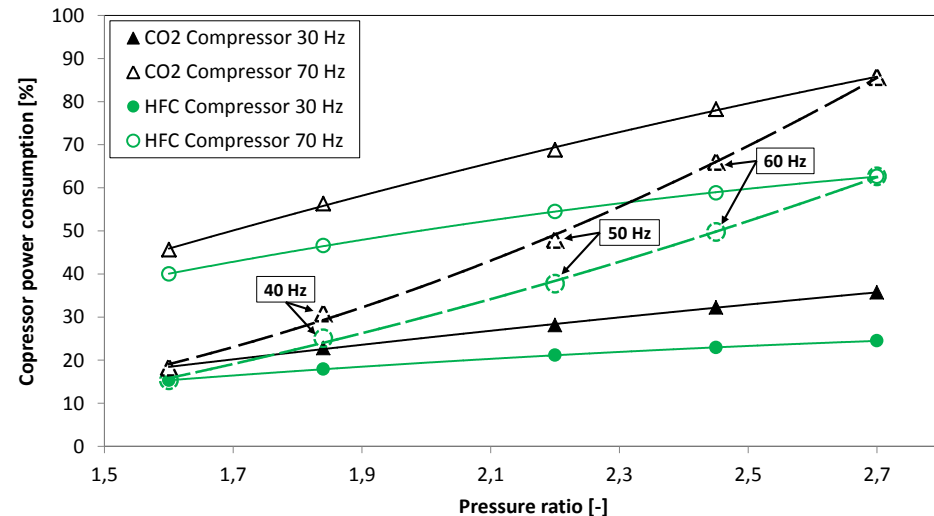
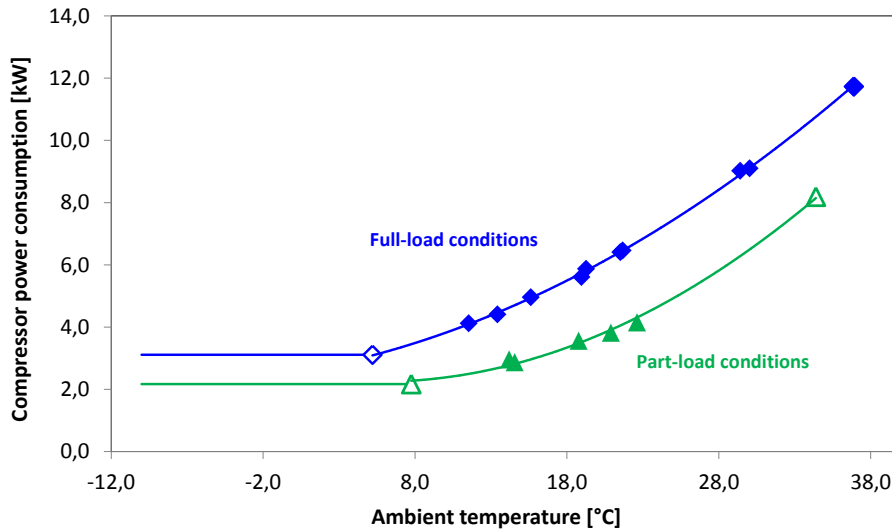
EXPERIMENTAL EVALUATION OF THE SEASONAL ENERGY EFFICIENCY RATING FOR A TRANS-CRITICAL R744 BOOSTER SYSTEM IN VARIOUS CLIMATE CONDITIONS

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Comparison of systems

Boundary conditions

Appendix A - Modelling Assumptions

Table A1: Assumptions – Thermodynamic Model (“State of Art” conditions)

Variable	Model 1		Model 2		Model 3		Model 4	
	MT	LT	MT	LT	MT	LT	MT	LT
Refrigerant	R404A	R404A	R404A	CO ₂	CO ₂	CO ₂	CO ₂	CO ₂
System type	DX	DX	DX	DX Cascade	Direct Expansion	DX	DX	DX Cascade
Cabinet cooling load (kW)	60	16	60	16	60	16	60	16
Cabinet air temperature (°C)	+2	-24	+2	-24	+2	-24	+2	-24
Evaporating temperature (°C)	-8	-36	-8	-32	-11	-32	-6 °C	-32
Head pressure control setting (saturated temperature, °C)	25	25	25	N/A	25	N/A	15	N/A
Cascade heat exchanger TD (K)	N/A	N/A	N/A	5	N/A	5	N/A	5
Condenser gas-cooler								
▪ Surface area (m ²)	340	110	470		500		260	
▪ Air flow rate (m ³ /s)	13	4	18	N/A	20	N/A	15	N/A
▪ Fan power (kW)	3.3	1.0	4.6		4.9		3.4	
Evaporator superheat (K)	5	5	5	5	5	5	5	5
Suction return temp (°C)	10	-5	10	-5	10	-5	10	-5
Suction line pressure drop (MPa)	0.013	0.013	0.013	0.013	0	0.013	0.013	0.013
Discharge line pressure drop (MPa)	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040
Liquid line pressure drop (MPa)	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040
Condenser outlet subcooling (K)	2	2	2	0	2	0	0.5	0

R134a
!

Insulation of receiver and liquid line, selection of EEX for small Δp

CO₂ booster

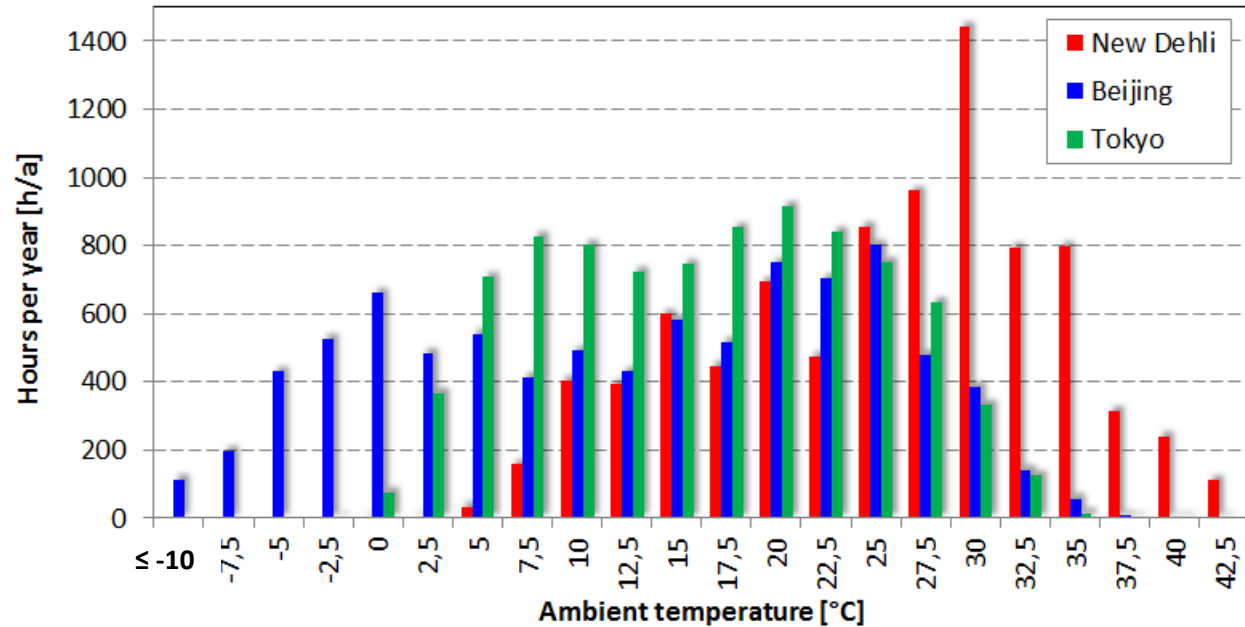
Full Load
MT: 14 kW
LT: 2 kW

tc min = 15 °C

HFC's: BITZER
NEW ECOLINE
VARISPEED
CO₂: VARISPEED
compressors in the
MT stage

Calculation of the annual efficiency

- / Applied weather data (ASHRAE 2009, Weather Data Viewer 4.0)
- / Results based on cooling capacity and power input of the compressors only
- / Annual efficiency based on a SEER calculation acc. to prEN 14825



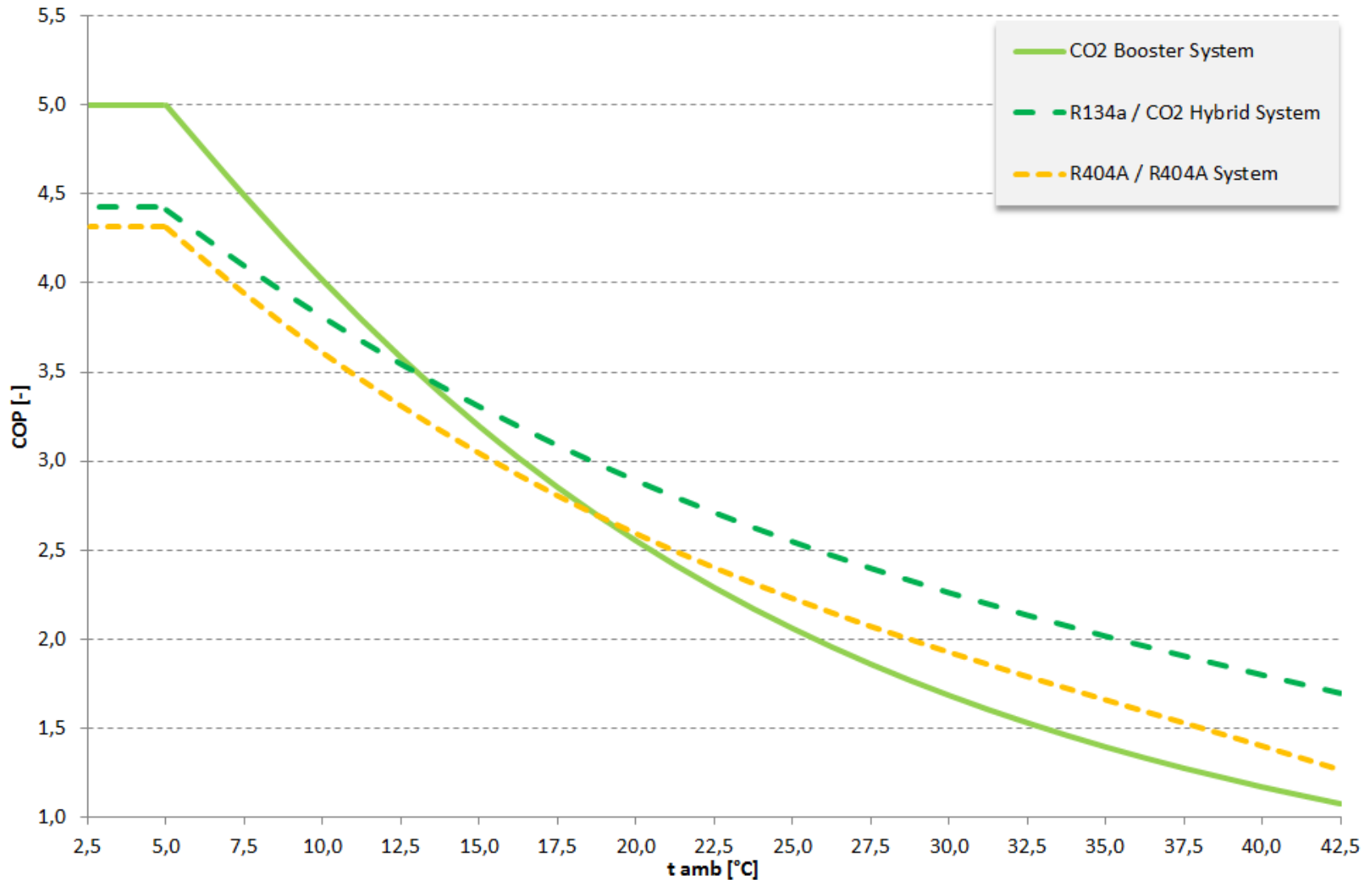
$$SEER = \sum_{j=1}^{22} \frac{Q(j) * h(j) * DG(j)}{P(j) * h(j)}$$

Results

Annual efficiency for Asian climates



COP as function of the ambient temperature



Summary



Summary

- / Classification of the annual efficiency of a state-of-the-art CO₂ booster system by an experimental and empirical study
- / Calculation of the annual efficiencies for optimized HFC systems
- / Out of the three solutions considered: An optimized hybrid system with R134a and CO₂ shows the best annual efficiencies in the chosen Asian climates
- / Applying a CO₂ booster system of the 3rd generation is beneficial for the discussed climates



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Thank you very much!